



## RECENT DEVELOPMENTS ON THE X-RAYS APPROACH TO HOLE-CUTTING

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## **OVERVIEW**

- Recent advances in automation
- A fast approximate wall distance function algorithm for initial hole boundary estimate
- A study on aerodynamic loads sensitivity to hole boundary locations
- Summary and conclusions

### **HOLE-CUTTING METHODS AND SOFTWARE** Ames Research Center

#### **Methods**

- Cartesian hole map
- Line of sight
- X-rays
- Implicit hole-cutting

#### **Software**

- PEGASUS5
- OVERFLOW/DCF
- SUGGAR++
- PUNDIT
- OVERTURE



**Object X-rays: Meakin, AIAA Paper 2001-2537** 

- Low memory









### **Automated**

- Closure of component open boundaries to provide proper X-ray pierce points pairing
- Determination of grid points to be cut by each X-ray
- Adaptive image plane map to handle components in close proximity
- Hole boundary adjustment to provide appropriate grid overlap

### Software

- Chimera Components Connectivity Library (C3LIB)
- Chimera Components Connectivity Program (C3P)
- Input: flow solver boundary conditions, component ID on solid walls
- Output: X-ray maps, hole point locations, fringe point interpolation stencils

Chan, W. M., Kim, N., Pandya, S. A., Advances in Domain Connectivity for Overset Grids Using the X-rays Approach, Paper ICCFD7-1201, 7th International Conference on Computational Fluid Dynamics, Big Island, Hawaii, July, 2012 (http://www.iccfd.org/iccfd7).

## **ADAPTIVE X-RAYS FOR MINIMUM HOLE**





## Ames Research Center AUTOMATED HOLE BOUNDARY ADJUSTMENT Minimum Hole Cut from Adaptive X-rays











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#### Ames Research Center AUTOMATED HOLE BOUNDARY ADJUSTMENT Orphan Removal Iterations



## After 1 step

After 3 steps



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#### Ames Research Center UNSTEADY 2-D HIGH-LIFT SYSTEM (SLAT REGION)





Spatially variable offset during relative motion simulation

## **OBJECTIVES OF CURRENT WORK**





Composite wall distance function is needed to cut holes between components on surface but was expensive to compute

Domain connectivity CPU time OVERFLOW/DCF = 68 sec. C3P = 107 sec. (54 sec. on computing composite wall distance function)

### Investigate faster algorithms

Manually specified or automatically created hole boundaries can have varying locations

Investigate sensitivities of aero load values and convergence rates





FUNCTION COMPUTATION (1)



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Construct uniform reference Cartesian grid around near-body volume grids Identify cut-cells for each component





## FAST APPROXIMATE COMPOSITE WALL DISTANCE FUNCTION COMPUTATION (2)



Determine accurate wall distance for vertices on cut-cells. Fill approximate wall distance for remaining vertices with Fast Marching Method

Interpolate wall distance from reference Cartesian grid onto original volume grids



# Not load balanced for connectivityOVERFLOW/DCF (original) – 8 MPI processesC3P (improved)– 8 OpenMP threads

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Test Case	# Grid pts (x10 <sup>6</sup> )	OVERFLOW/DCF	СЗР
XV-15	10.0	0.8 min.	0.7 min. ( <mark>-12.5%</mark> )
DPW4	16.8	1.2 min.	1.5 min. ( <mark>+25%</mark> )
2 Rockets	24.5	1.0 min.	0.6 min. ( <mark>-40%</mark> )
D8	77.7	11.5 min.	6.0 min. ( <mark>-48%</mark> )

Number of wall-distance function computations needed for connectivity

OVERFLOW/DCF	C3P
0	Ν

N = number of components



## **AERODYNAMIC LOADS SENSITIVITY STUDY**

## **Objectives**

Investigate correlation between component aerodynamic loads (values and convergence) with

- hole boundary offset distance
- cell attribute compatibility between fringe point and interpolation stencil

## Approach

- Define a normalized hole boundary offset distance and a cell attribute compatibility measure
- Compute solution on test cases with different normalized hole boundary offset distances
  - Single capsule
  - Two rockets
  - 4<sup>th</sup> AIAA Drag Prediction Workshop Common Research Model
  - D8 Double Bubble Aircraft





## NORMALIZED HOLE BOUNDARY OFFSET DISTANCE

#### Hole in off-body grids

Define normalized hole boundary offset distance  $\delta = D_h / D_b$ 

#### Hole in near-body grids

Define similar  $\delta$  based on min distance between components



 $\delta = 0.0$ 

 $\delta = 0.5$ 







## **CELL ATTRIBUTE COMPATIBILITY**

Possible measures: cell volume, aspect ratio, orientation

**Current simple measure:** 

Let V<sub>f</sub> = cell volume at fringe point V<sub>i</sub> = cell volume at interpolation stencil



Local compatibility measure  $c = min(V_f/V_i, V_i/V_f)$ 

Global cell size compatibility *C* = average *c* over all fringe points (orphan points get value zero)

(all fringes are orphans)  $0 \le C \le 1$  (ideal compatibility)



## **SINGLE CAPSULE** M=1.2, α=180.0, Re/in.=18200



## C3P hole boundary



#### Drag coefficient convergence history



# Converged value variation from $\delta$ =0.5: -0.3% to +0.5%

**Convergence is similar for all cases** 







![](_page_20_Picture_0.jpeg)

# Ames Research Center AIAA 4<sup>TH</sup> DRAG PREDICTION WORKSHOP CRM Grid and Solution (M=0.85, α=2.363 deg., Re/in.=18129.08)

Hole Boundaries from C3P

**Pressure Coefficient** 

![](_page_21_Figure_3.jpeg)

![](_page_22_Figure_0.jpeg)

![](_page_23_Figure_0.jpeg)

![](_page_24_Picture_0.jpeg)

![](_page_24_Figure_1.jpeg)

![](_page_25_Picture_0.jpeg)

## **D8 DOUBLE BUBBLE AIRCRAFT** $C_L$ , $C_D$ , $C_M$ Convergence Histories and

![](_page_25_Picture_2.jpeg)

**Deviations from Group Mean for \delta=0.25, 0.5, 0.75 and C3P** 

![](_page_25_Figure_4.jpeg)

Time step number

![](_page_26_Figure_0.jpeg)

![](_page_27_Picture_1.jpeg)

## **SUMMARY AND CONCLUSIONS**

#### **Enhanced X-rays - C3P software**

- Inputs only require flow solver b.c. and component tags on walls
- Automated efficient treatment of components in close proximity
- Automated spatially variable hole boundary offset from minimum hole

#### **Fast Wall Distance Function Computation**

- CPU time mostly comparable to OVERFLOW/DCF (original X-rays)
- Benefits more significant if usable for solving turb. model equations

### Aerodynamic Loads Sensitivity Study

- Similar aero load convergence rates observed for all  $\delta\mbox{'s}$  and C3P
- For best practice hole boundary offset distances ( $\delta$  = 0.25 0.75), aero load converged values do not appear to correlate with  $\delta$  or cell size compatibility
- Typical variations of aero loads for  $\delta = 0.25 0.75$  and C3P are small relative to typical variations between different flow solvers, grid stretching ratios, turbulence models